2N4151 (SILICON) thru 2N4198

2N4151 thru 2N4198 (continued)

ELECTRICAL CHARACTERISTICS ($T_C = 25^{\circ}$ C unless otherwise noted)

(1) Ratings apply for zero or negative gate voltage. These devices should not be tested with a constant current source for forward or reverse
blocking capability such that the voltage applied exceeds the rated blocking vol

(2) For optimum operation, i.e. faster turn-on, lower switching losses, best di/dt capability, recommended $I_{GT} = 200$ mA minimum. -Indicates JEDEC Registered Data

TYPICAL TRIGGER CHARACTERISTICS

CURRENT DERATING

FIGURE 4 - MAXIMUM AMBIENT TEMPERATURE

IT(AV), AVERAGE FORWARD CURRENT (AMP)

FIGURE 6 - MAXIMUM SURGE CAPABILITY

NUMBER OF CYCLES

FIGURE 8 - FORWARD VOLTAGE

FIGURE 10 - TYPICAL THERMAL RESISTANCE OF PLATES

FIGURE 9 - HOLDING CURRENT

FIGURE 11 - CASE-TO-AMBIENT THERMAL RESISTANCE

MOUNTING and THERMAL INFORMATION

where:

The versatility of the Motorola SCR can-type package
affords a variety of mounting methods to meet individual re-
quirements. Depending upon the thermal resistance value be-
tween the SCR case and a heat sink, any mounting

recommendations apply:

- A. Heat Sink Contact
	- 1. Since the silicon die is located in the case bottom, (opposite end from tubed header point A as shown on the mechanical outline drawing, Figure 12.) the heat sink contact should be made with case bottom for proper heat transfer.
- B. General Soldering Precautions
	- 1. Solder -- Use solder with melting points between
+175°C and +225°C. The commonly-used tin-lead
alloy solders have melting points of +188°C (60/40
alloy) and +214°C (50/50 alloy).
	- 2. Flux (when used) Non-corrosive resin preferred.
	- 3. When soldering to the device terminals or leads,use of a heat dissipator between soldering point and SCR case is recommended.
- C. Case Soldering Methods
	- 1. Heat Sink Materials:
		- a. Copper and most of its alloys present no problem in soldering and would probably be the most favorable heat sink material.
b. Stainless steel is difficult to solder. However, us
		- ing a strong acid-filled solder, satisfactory soldering can be achieved.
		- c. In most cases where soldering is difficult, such as with aluminum, proper preparation with a tin coat- ing on the material can bring about good results.

Depending on specific needs, soldering can be effected by using either hot plate, oven, or belt feed furnace_ In all cases, temperature must be controlled.

- 2. Hot Plate The hot plate is probably the most effec-tive and flexible method of soldering. The following method is recommended:
	- a. Set surface temperature of hot plate to a maxi-mum of 225·C.
	- b. Place heat sinks on hot plate for approximately 5 **minutes.**
	- c. Place $\frac{1}{8}$ "- $\frac{1}{4}$ " diameter solder preform on area of heat sink to be soldered.
	- d. After solder becomes liquid, place device on this area applying slight pressure and rotating the device slightly to assure good contact. Flux may be
used here if required. Frequently, suitable wetting
can be achieved mechanically when the device is rotated in the liquid solder, depending upon the device surface conditions.
	- e. Remove heat sinks from heat source and free air cool.
- 3. Oven When soldering is performed in an oven, use
a solder preform (disc, 0.300" x 0.010") or flatten
solder wire ($V_8V^{-1}V_a$ ") before placing it on the heat
sink. For an inert atmosphere such as N_n, dry air,
etc., used, flux should not be required. Again, temperature must be controlled.
- 4. Belt Feed Furnace The procedures are much the same as with the oven method, with the exception that possibly a jig would be required to hold the device and the heat sink in the proper position.
-
- D. Epoxy Mounting Suggestions
1. There are many good commercial epoxies available
today, such as Hysol's "HY-TAC" kit or 3M's
"Scotch Cast #9". Suitable mounting may be ob-
tained by following the epoxy manufacturer's recthyristor to the mounting surface with a slight pres-
sure and rotary movement. If improved thermal
conductivity is desired, powdered alumina (325
mesh) may be mixed into the epoxy in a proportion
of 70% (epoxy) to 30% (al sink, thin fiberglass tape (course surface) or mica discs may be used.

The primary reason for specifying mounting details is to
help maintain the junction temperature of the SCR at a safe
level and hence provide satisfactory operation. The funda-
mental relationship between junction temperatu sinks can be expressed as follows:

$$
T_J = T_A + R\theta_{JA} P_D
$$

 T_J = junction temperature (100°C max operating for these devices)

 $T_A =$ ambient temperature

- $B\theta_{JA} =$ junction-to-ambient thermal resistance $=$ R θ _{JC} + R θ _{CA} (with R θ _{CA} = R θ _{CS} + R θ _{SA} when
	- heat sink used)
- $B\theta_{JC}$ = junction-to-case thermal resistance
- $R\theta_{\text{CA}}$ = case-to-ambient thermal resistance
- $R\theta_{CS}$ = case-to-heat sink thermal resistance
- $\texttt{R}\theta\texttt{SA} = \texttt{heat}$ sink-to-ambient thermal resistance
	- $P_D =$ average power dissipated in the SCR

It is more accurate to base circuit designs upon the case temperature. The preferred method to determine case temperature is to place a thermocouple on the package at point A as shown on the mechanical outline drawing. Figure 12. Even when used in free air. the mass of ,the package is large enough so that it will not respond to heat surges generated at a 60 Hz rate or higher once steady-state conditions are achieved.

For operation with a heat sink, normally, the Rθ_{CS} portion of Rθ_{CA} will range between 0.2 and 1⁰ C/W for the can type SCR's, depending upon the particular mounting. $\textsf{R}\theta_\textsf{CA}$ is approximately 0.2° C/W for the stud packages when used with a thermal grease. Likewise, the R θ SA portion of R θ CA will vary with the shape, **material, and configuration of the heat sink as well as with the** surrounding conditions. Figure 10 is a very basic guide to $\text{R}\theta_\text{SA}$.

For free air operation, in instances where the case temperature cannot be measured or for preliminary engineering work, the case temperature can be estimated by using values of case-to-ambient thermal resistance, obtained from Figure 11 and the relation:

 $T_C = R \theta_{CA} P_D + T_A$
The graph of Figure 11 indicates that the lead length of the SCR and the thermal mass of the connection to the lead will influence the value of $R\theta_{CA}$.

For convenience, Figure 4 shows derating information when the parts are in a still air ambient mounted on a typical P.C. board.

2N4151 thru 2N4198 (continued)

(1) GATE
2 CATHOL **CATHODE ANODE**

1. The case (anode) leads for the 2N4183·90 and 2N4191·98 series may be attached by either soldering or welding techniques.

2. On all package types: Manufacturer may optionally use
a small metal tab on the case perimeter opposite the gate
terminal for terminal identification purposes.

3. Point A indicates temperature reference pOint