# BY 126 BY 127

## "SURMETIC" RECTIFIERS

 $\ldots$  subminiature size, axial lead mounted rectifiers for general purpose low-power applications.

## LEAD MOUNTED SILICON RECTIFIERS

### DIFFUSED JUNCTION

### **MAXIMUM RATINGS**

| Characteristic   | Symbol   | BY126            | BY127 | Unit  |
|--|--|------------------|-------|-------|
| Peak Repetitive Reverse Voltage<br>Working Peak Reverse Voltage<br>DC Blocking Voltage                             | V <sub>RM(rep)</sub><br>V <sub>RM(wkg)</sub><br>V <sub>R</sub> | 450              | 800   | Volts |
| Non-Repetitive Peak Reverse Voltage<br>(halfwave, single phase, 60 Hz peak)  | V <sub>RM(non-rep)</sub>                                       | 650              | 1250  | Volts |
| RMS Reverse Voltage  | v <sub>r</sub>   | 315              | 560   | Volts |
| Average Rectified Forward Current<br>(single phase, resistive load,<br>60 Hz, see Figure 6, T <sub>A</sub> = 75°C) | IO   | 1.0              |       | Amp   |
| Non-Repetitive Peak Surge Current<br>(surge applied at rated load<br>conditions, see Figure 2)                     | IFM(surge)   | 40 (for 1 cycle) |       | Amp   |
| Operating and Storage Junction<br>Temperature Range  | T <sub>J</sub> , T <sub>stg</sub>                              | -65 to +175      |       | °C    |



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## **ELECTRICAL CHARACTERISTICS**

| Characteristic and Conditions   | Symbol             | Max   | Unit  |
|---|--------------------|-------|-------|
| Maximum Instantaneous Forward Voltage Drop<br>(i <sub>F</sub> = 1, 0 Amp, T <sub>J</sub> = 25°C) Figure 1 | v <sub>F</sub>     | 1. 1  | Volts |
| Maximum Full-Cycle Average Forward Voltage Drop ( $I_O = 1.0$ Amp, $T_L = 75$ °C. 1 inch leads)           | V <sub>F(AV)</sub> | 0,8   | Volts |
| Maximum Reverse Current (rated dc voltage) $T_J = 25$ °C  | I <sub>R</sub>     | 0.01  | mA    |
|   | I <sub>R(AV)</sub> | 0. 03 | mA    |



CASE: Void free, Transfer Molded

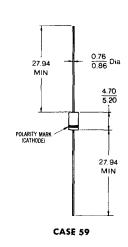
MAXIMUM LEAD TEMPERATURE FOR SOLDERING PURPOSES: 350°C, 3/8" from

case for 10 seconds at 5 lbs. tension

FINISH: All external surfaces are corrosion-resistant, leads are readily solderable

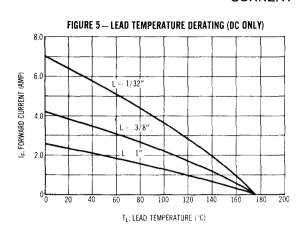
POLARITY: Cathode indicated by color band

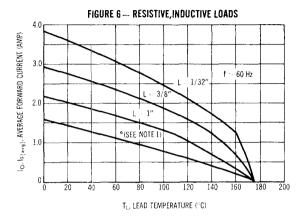
WEIGHT: 0.40 Grams (approximately)

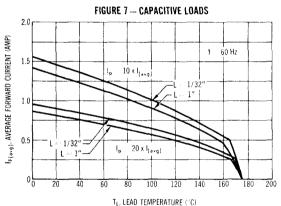


Dimensions in millimeters

#### CURRENT DERATING DATA



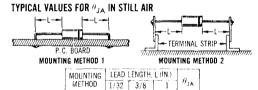




## NOTES

#### NOTE 1

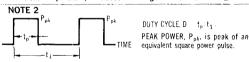
Data shown for thermal resistance junction to ambient  $(H_{JA})$  for the mountings shown is to be used as typical guideline values for preliminary engineering or in case the tie point temperature cannot be measured.



°Using Mounting Method 1 or 2 with L=1'' the curve marked ° in Figure 6 can be used for 60 Hz half-wave resistive/inductive load (Rating vs. Ambient Temperature). The abscissa of Figure 6 then indicates  $T_{\rm A}$  in °C.

75 85

C/W



55 72 85 C/W

To determine maximum junction temperature of the diode in a given situation, the following procedure is recommended:

The temperature of the lead should be measured using a thermocouple placed on the lead as close as possible to the tie point. The thermal mass connected to the tie point is normally large enough so that it will not significantly respond to heat surges generated in the diode as a result of pulsed operation once steady-state conditions are achieved. Using the measured value of  $T_{\rm L}$ , the junction temperature may be determined by:

$$T_J = T_L \pm \triangle T_{JL},$$

where  $\lesssim T_{JL}$  is the increase in junction temperature above the lead temperature. It may be determined by:

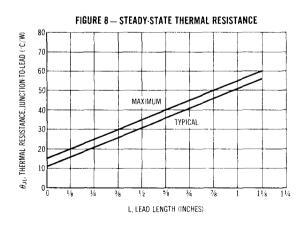
$$\triangle T_{JL} \cong P_{pk} \left[ \left. \theta_{JL(\infty)} \bullet D \oplus (1-D) \bullet \theta_{JL(t_1+|t_p|)} + \theta_{JL(t_p)} - \theta_{JL(t_1)} \right] \right]$$

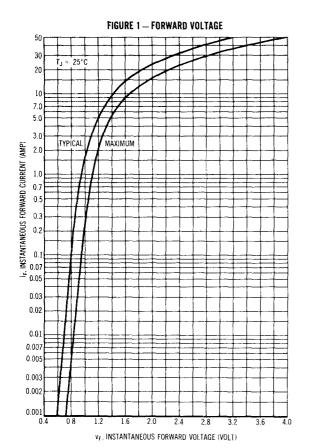
where  $\theta_{JU(t)} = \text{value of transient thermal resistance at time t, i.e.:}$ 

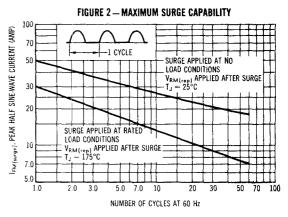
 $\theta_{\mathsf{JL}(\mathsf{t_1}+\mathsf{t_p})} = \mathsf{value} \; \mathsf{of} \; \theta_{\mathsf{JL}(\mathsf{t})} \; \mathsf{at} \; \mathsf{time} \; \mathsf{t_1} + \mathsf{t_p}$ 

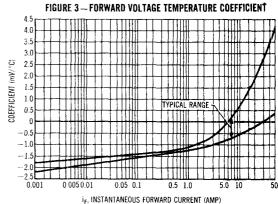
 $\theta_{JL\{t_{\mathbf{p}}\}} = \text{value of } \theta_{JL\{t\}} \text{ at end of pulse width } t_{\mathbf{p}}$ 

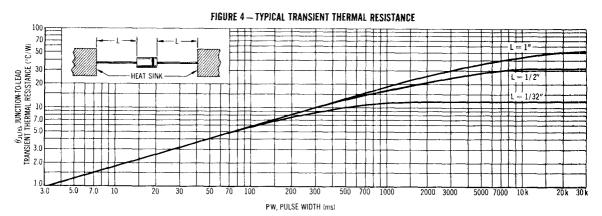
 $\theta_{JL\{t_1\}} = \text{value of } \theta_{JL\{t\}} \text{ at time } t_1$ 











FOR  $\theta_{JL(1)}$  VALUES AT PULSE WIDTHS LESS THAN 3.0 ms, THE ABOVE CURVE CAN BE EXTRAPOLATED DOWN TO 10  $_{I^{\rm LS}}$  AT A CONTINUING SLOPE OF 1/2

#### TYPICAL DYNAMIC CHARACTERISTICS



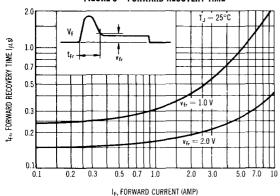
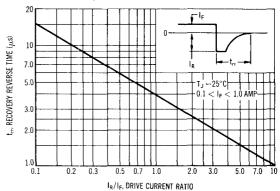


FIGURE 10 - REVERSE RECOVERY TIME



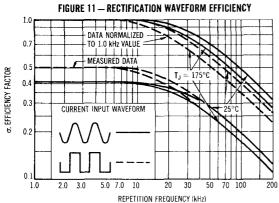
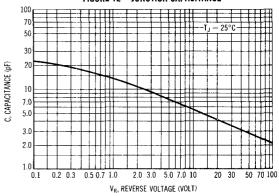
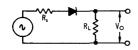


FIGURE 12 - JUNCTION CAPACITANCE



## RECTIFIER EFFICIENCY NOTE

### FIGURE 13 - SINGLE-PHASE HALF-WAVE RECTIFIER CIRCUIT



$$\sigma_{\text{(sine)}} = \frac{\frac{V_{\text{m}}^2}{\pi^2 R_{\text{L}}}}{\frac{V_{\text{m}}^2}{4R_{\text{L}}}} \cdot 100\% = \frac{4}{\pi^2} \cdot 100\% = 40.6\%$$
 (2)

For a square wave input of amplitude  $\boldsymbol{V}_{m},$  the efficiency factor becomes:

$$\sigma_{\text{(square)}} = \frac{\frac{V_{m}^{2}}{2R_{L}}}{\frac{V_{m}^{2}}{R_{L}}} \cdot 100\% = 50\%$$
 (3)

(A full wave circuit has twice these efficiencies)

As the frequency of the input signal is increased, the reverse recovery time of the diode (Figure 10) becomes significant, resulting in an increasing ac voltage component across  $R_L$  which is opposite in polarity to the forward current, thereby reducing the value of the efficiency factor  $\sigma_r$  as shown on Figure 11.

It should be emphasized that Figure 11 shows waveform efficiency only; it does not provide a measure of diode losses. Data was obtained by measuring the ac component of  $V_{\rm O}$  with a true rms ac voltmeter and the dc component with a dc voltmeter. The data was used in Equation 1 to obtain points for Figure 11.

The rectification efficiency factor  $\sigma$  shown in Figure 11 was calculated using the formula:

$$\sigma = \frac{P_{de}}{P_{rms}} = \frac{\frac{V_{O}^{2}(dc)}{R_{L}}}{\frac{V_{O}^{2}(rms)}{R_{L}}} \cdot 100\% = \frac{V_{O}^{2}(dc)}{V_{O}^{2}(ac) + V_{O}^{2}(dc)} \cdot 100\% \quad (1)$$

For a sine wave input  $V_m \sin (\omega t)$  to the diode, assumed lossless, the maximum theoretical efficiency factor becomes: